TITLE OF THE INVENTION

Compressor Piston and Process for Producing the Compressor Piston

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BACKGROUND OF THE INVENTION

The present invention relates to compressor pistons, and more specifically, to hollow pistons and a process for producing hollow pistons.

A typical variable displacement compressor is provided with a tilting swash plate, which is located in a crank chamber, and pistons are connected to the swash plate. The swash plate converts rotational motion of a drive shaft into reciprocating motions of the pistons. The inclination angle of the swash plate varies depending on the pressure in the crank chamber. The inclination angle of the swash plate governs the piston stroke and displacement of the compressor.

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Japanese Unexamined Patent Publication Nos. Hei 10-281065, Hei 11-294320 and Hei 11-107912 each disclose a hollow piston to be used in a compressor. Hollow pistons are light and have small inertia forces. Therefore, if hollow pistons are used in a variable displacement compressor, they minimize their influence on the swash plate's movement of changing the inclination angle, so that the displacement of the compressor can be changed with good response.

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The thinner the wall of the piston is, the lighter the piston is. However, when a piston compresses refrigerant gas, the end wall of the piston head receives the high pressure of the compressed refrigerant gas. A typical piston has a flat head end wall, so that if the head end wall is relatively

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thin, it cannot withstand the pressure.

The piston disclosed in Japanese Unexamined Patent Publication No. Hei 10-281065, which is referred to above, has a recess at the center of the head end wall. When the piston is machined, a center pin of a machine tool is fitted in the reference recess. The machine tool cuts the periphery of the piston while the piston rotates around the a rotational axis.

The recess reduces the strength of the head end wall of the piston. To improve the strength of the head end wall, the thickness of the wall must be increased. However, this increases the weight of the piston.

BRIEF SUMMARY OF THE INVENTION

It is an objective of the present invention to provide a light and strong hollow piston and a process for producing a hollow piston.

To achieve the above objective, the present invention provides a hollow piston used in a compressor. The piston has an end wall that receives the pressure of a cylinder bore of the compressor. The end wall has a substantially flat outer end face and an inner end face that is opposite to the outer end face. The contour of the inner end face, from the radially outside portion toward the radially inside portion, first approaches the outer end face and then departs from the outer end face.

The present also provides another hollow piston used in a compressor. The piston is accommodated in a cylinder bore of the compressor. The piston includes an end wall that receives the pressure of the cylinder bore. The end wall has a

substantially flat outer end face and an inner end face that is opposite to the outer end face. A recess is formed in the outer end face. A protrusion is formed on the inner end face to reinforce the end wall.

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Further, the present invention may be applied to a method for manufacturing a hollow piston used in a compressor. piston includes a head piece and a body piece that is coupled to the head piece. The head piece includes an end wall that receives the pressure of a cylinder bore of the compressor and the body piece includes the remainder of the piston. The end wall includes a substantially flat outer end face and an inner end face that is opposite to the outer end face. The method includes preparing a mold for forming the head piece, wherein the mold is designed such that a temporary protrusion that is not present in the finished head piece is formed on the inner end face, pouring molten metal into the mold, pushing the temporary protrusion before the molten metal solidifies to prevent formation of shrinkage cavities and removing the protrusion after the molten metal solidifies.

Other aspects and advantages of the invention will become apparent from the following description, taken in conjunction with the accompanying drawings, illustrating by way of example the principles of the invention.

BRIEF DESCRIPTION OF SEVERAL VIEWS OF THE DRAWING

The invention, together with objects and advantages thereof, may best be understood by reference to the following description of the presently preferred embodiments together with the accompanying drawings in which:

Fig. 1 is an overall cross-sectional view of a compressor according to a first embodiment of the present invention;

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Fig. 2 is a cross-sectional view of a piston incorporated into the compressor shown in Fig. 1;

Fig. 3 is a cross-sectional view taken along the line 3-3 in Fig. 2;

Fig. 4 is a cross-sectional view taken along the line 4-4 in Fig. 2;

Fig. 5 is a cross-sectional view of a piston according to a second embodiment of the present invention;

Fig. 6 is a cross-sectional view of a piston according to a third embodiment of the present invention;

Fig. 7 is a cross-sectional view of a piston according to a fourth embodiment of the present invention;

Fig. 8 is a cross-sectional view taken along the line 8-8 in Fig. 7;

Fig. 9(a) is a cross-sectional view of a piston according to a fifth embodiment of the present invention;

Fig. 9(b) is a cross-sectional view taken along the line 9(b)-9(b) in Fig. 9(a);

Fig. 10(a) is a cross-sectional view of a piston according to a sixth embodiment of the present invention;

Fig. 10(b) is a cross-sectional view taken along the line 10(b)-10(b) in Fig. 10(a);

Fig. 11(a) is a cross-sectional view of a piston according to a seventh embodiment of the present invention;

Fig. 11(b) is a cross-sectional view taken along the line 11(b)-11(b) in Fig. 11(a);

Fig. 12(a) is a cross-sectional view of a piston according to an eighth embodiment of the present invention;

Fig. 12(b) is a cross-sectional view taken along the line 12(b)-12(b) in Fig. 12(a);

Fig. 13(a) is a cross-sectional view of a piston according to a ninth embodiment of the present invention;

Fig. 13(b) is a cross-sectional view taken along the line 13(b)-13(b) in Fig. 13(a);

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Fig. 14(a) is a cross-sectional view of a piston according to a tenth embodiment of the present invention;
Fig. 14(b) is a cross-sectional view taken along the line

14(b)-14(b) in Fig. 14(a);

Fig. 15(a) is a cross-sectional view of a piston according to an eleventh embodiment of the present invention;

Fig. 15(b) is a cross-sectional view taken along the line 15(b)-15(b) in Fig. 15(a);

Fig. 16(a) is a cross-sectional view of a piston according to a twelfth embodiment of the present invention;
Fig. 16(b) is a cross-sectional view taken along the line

16(b)-16(b) in Fig. 16(a);

Fig. 17(a) is a cross-sectional view of a piston according to a thirteenth embodiment of the present invention;
Fig. 17(b) is a cross-sectional view taken along the line 17(b)-17(b) in Fig. 17(a);

Fig. 18(a) is a cross-sectional view of a piston according to a fourteenth embodiment of the present invention;

Fig. 18(b) is a cross-sectional view taken along the line 18(b)-18(b) in Fig. 18(a);

Fig. 19 is a cross-sectional view of a piston according to a fifteenth embodiment of the present invention;

Fig. 20 is a cross-sectional view taken along the line 20-20 in Fig. 19;

25 Fig. 21 is a cross-sectional view of a piston according to a sixteenth embodiment of the present invention;

Fig. 22 is a cross-sectional view taken along the line 22-22 in Fig. 21;

Fig. 23(a) is a cross-sectional view showing a state where a molten metal is poured into a mold; and

Fig. 23(b) is a cross-sectional view for illustrating how the protrusion is cut.

DETAILED DESCRIPTION OF THE PREFERRED EMBODIMENTS

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The first embodiment will be described below with reference to Figs. 1 to 4. As shown in Fig. 1, a variable displacement compressor is provided with a cylinder block 11, a front housing member 12 connected to the front end of the cylinder block 11 and a rear housing member 19 connected to the rear end of the cylinder block 11. The front housing member 12 defines a controlled pressure chamber 121. The rear housing member 19 defines a suction chamber 191 and a discharge chamber 192.

A drive shaft 13 is supported by the front housing member 12 and the cylinder block 11. The drive shaft 13 is driven by an external drive source, for example, an engine. A rotary support 14 is located in the controlled pressure chamber 121 and is fixed to the drive shaft 13. A drive plate, or swash plate 15, is located in the controlled pressure chamber 121 and is supported by the drive shaft 13. The swash plate 15 can slide along the drive shaft 13 in the axial direction and can incline with respect to a plane that is perpendicular to the axis of the drive shaft 13.

A pair of guide pins 16 extend from the swash plate 15 and are loosely fitted in a pair of guide holes 141, which are formed in the rotary support 14. A hinge mechanism, which includes the guide pins 16 and the guide holes 141, drives the swash plate 15 integrally with the drive shaft 13. The hinge mechanism also permits the swash plate 15 to slide and incline with respect to the drive shaft 13.

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The controlled pressure chamber 121 communicates with the suction chamber 191 through a bleed passage (not shown). The discharge chamber 192 communicates with the controlled pressure chamber 121 through a supply passage (not shown). A

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displacement control valve 25 is located in the supply The control valve 25 adjusts the flow rate of refrigerant gas supplied from the discharge chamber 192 to the controlled pressure chamber 121 to control the pressure in the chamber 121. An increase in the quantity of the refrigerant gas supplied from the discharge chamber 192 to the controlled pressure chamber 121 will increase the pressure in the controlled pressure chamber 121. A decrease in the flow rate of the refrigerant gas supplied from the discharge chamber 192 to the controlled pressure chamber 121 will decrease the pressure in the controlled pressure chamber 121. inclination angle of the swash plate 15 varies depending on the pressure in the controlled pressure chamber 121. increase in the pressure in the controlled pressure chamber 121 will decrease the inclination angle of the swash plate 15. A decrease in the pressure in the controlled pressure chamber 121 will increase the inclination angle of the swash plate 15.

As shown in Fig. 1, when the swash plate 15 abuts against the rotary support 14, the swash plate 15 is positioned at the maximum inclination angle position. When the swash plate 15 abuts against a snap ring 24, which is fitted on the drive shaft 13, the swash plate 15 is positioned at the minimum inclination angle position.

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The cylinder block 11 contains a plurality of cylinder bores 111 (only two cylinder bores are shown in Fig. 1) arranged around the axis of the drive shaft 13. Each cylinder bore 111 contains an aluminum piston 17. Each piston 17 is connected to the swash plate 15 through a pair of shoes 18. The swash plate 15 converts the rotational motion of the drive shaft 13 into reciprocating motion of the pistons 17. The inclination angle of the swash plate 15 governs the strokes of the pistons 17 and the displacement of the compressor.

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A port plate 20, a suction valve plate 21, a discharge valve plate 22 and a retainer plate 23 are located between the cylinder block 11 and the rear housing member 19. Formed in the port plate 20 are suction ports 201 and discharge ports 202 for the respective cylinder bores 111. The suction valve plate 21 has suction valve flaps 211 for the respective suction ports 201. The discharge valve plate 22 has discharge valve flaps 221 for the respective discharge ports 202. The retainer plate 23 has retainers 231 for the respective discharge valve flaps 221.

When a piston 17 travels from top dead center to bottom dead center, the refrigerant gas in the suction chamber 191 flows through the suction port 201 and by the suction valve flap 211 into the corresponding cylinder bore 111. When the piston 17 travels from the bottom dead center to the top dead center, the refrigerant gas is compressed in the corresponding cylinder bore 111, and the compressed refrigerant gas is discharged through the discharge port 202 and by the discharge valve flap 221 into the discharge chamber 192. The travel of the discharge valve flap 221 is limited by the retainer 231.

An external refrigerant circuit 26 connects the discharge chamber 192 to the suction chamber 191. The external refrigerant circuit 26 contains a condenser 27, an expansion valve 28 and an evaporator 29. The refrigerant flowing from the discharge chamber 192 into the external refrigerant circuit 26 flows through the condenser 27, the expansion valve 28 and the evaporator 29 into the suction chamber 191.

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As shown in Figs. 2 and 3, each piston 17 includes a cavity 171. The piston 17 has a head piece 31 and a body piece 32, which are joined to one another. The head piece 31 has a substantially flat head end wall 30 and an annular rim

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35, which is formed on the rear side of the head end wall 30. The head end wall 30 receives the pressure in the corresponding cylinder bore 111. The body piece 32 includes a cylindrical wall 34, which defines the cavity 171, and a skirt 33, which extends from the rear end of the cylindrical wall 34. The skirt 33 has a pair of receiving recesses 331 for receiving the shoes 18, respectively.

The annular rim 35 is fitted in the open end of the cylindrical wall 34, and the head and body pieces 31 and 32 are welded to each other. The head piece 31 serves as a cap for closing the opening of the body piece 32. The inner wall surface 341 and outer wall surface 342 of the cylindrical wall 34 and the inner wall surface 351 and outer wall surface 352 of the annular rim 35 are coaxial with the axis L of the piston 17.

The head end wall 30 has a flat outer end face 36, which faces and is parallel to the suction valve plate 21. A positioning recess 361, which is centered on the axis L is formed on the outer end face 36. As described in Japanese Unexamined Patent Publication No. Hei 10-281065 in the background section, the positioning recess 361 is used to cooperate with a center pin of a machine tool for cutting the outer surface of the piston 17. Also, when the piston 17 is incorporated into a cylinder bore 111, a positioning jig engages with the positioning recess 361.

The head end wall 30 has an inner end face 37 facing the cavity 171. The inner end face 37 includes an annular concave portion 371 and a convex portion 372, which is radially inside the concave portion 371. The annular concave portion 371 and the convex portion 372 define a protrusion 50 for reinforcing the head end wall 30.

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Fig. 2 shows a cross-sectional view of the piston 17, which is cut along the plane S (see Fig. 4). An outer arcuate line 373, which is shown in Fig. 2, is a generatrix of the annular concave portion 371. That is, the annular concave portion 371 is formed by rotating the outer arcuate line 373 once around the axis L. An inner arcuate line 374, which is shown in Fig. 2, is a generatrix of the convex portion 372. That is, the convex portion 372 is formed by rotating the inner arcuate line 374 once around the axis L. The convex portion 372 is a part of a sphere.

The radius of the outer arcuate line 373 is smaller than that of the inner arcuate line 374. The outer arcuate line 373 connects smoothly to the inner surface 351 of the annular rim 35. The inner arcuate line 374 smoothly meets the outer arcuate line 373. In other words, the annular concave portion 371 smoothly meets the inner wall surface 351 of the annular rim 35, and the convex portion 372 smoothly meets the annular concave portion 371. Both the annular concave portion 371 and the convex portion 372 are coaxial with the axis L.

An imaginary circle K, which is shown by a broken line, illustrates the boundary between the annular concave portion 371 and the convex portion 372. The annular concave portion 371 is radially outside imaginary circle K, and the convex portion 372 is radially inside the imaginary circle K. The convex portion 372 is coaxial with the positioning recess 361. In other words, the convex portion 372 is aligned axially with the positioning recess 361.

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The first embodiment has the following advantages.

The contour of the inner end face 37 of the head end wall 30, from the inner wall surface 351 toward the axis L, first

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approaches the outer end face 36 and then departs from it. In other words, the annular concave portion 371 smoothly joins to the inner wall surface 351 of the annular rim 35, and the convex portion 372 smoothly joins the annular concave portion 371. This configuration prevents the concentration of stress between the inner end face 37 of the head end wall 30 and the inner wall surface 351 of the annular rim 35.

The annular concave portion 371 and the convex portion 372 define the protrusion 50. The protrusion 50 has a smooth surface to prevent local stress concentration. The combination of the annular concave portion 371 and the convex portion 372 has an excellent stress deconcentrating effect compared with a simple plate-like head end wall and can reduce the quantity of the material needed to form the head end wall 30 while providing the required strength. This contributes to reducing the weight of the piston 17.

The convex portion 372 is aligned axially with the positioning recess 361. The center of the convex portion 372, which is axially aligned with the positioning recess 361, is farthest from the outer end face 36. In other words, the convex portion 372 most effectively reinforces the portion of the head end wall 30 where the positioning recess 361 is located. Thus, the wall around the positioning recess 361 is strong. The convex portion 372 is formed in the portion of the head end wall 30 that is to be reinforced most. This improves the strength and reduces the weight of the head end wall 30.

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The head piece 31 is formed by die casting, cutting or press molding. When the head piece 31 and the body piece 32 are separated from each other, the inner end face 37 of the head end wall 30 is exposed. Thus, the two part structure

facilitates shaping of the inner end face 37 of the head end wall 30.

Next, a second embodiment of the present invention will be described with reference to Fig. 5 mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. In this embodiment, the head piece 31 is fitted in the body piece 32 such that the head 31 is entirely fitted within the cylindrical wall 34, as shown in Fig. 5.

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A third embodiment of the present invention will be described with reference to Fig. 6 mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. In this embodiment, a cylindrical rim 350 corresponding to the cylindrical wall 34 in Fig. 2 is formed integrally with the head piece 31, as shown in Fig. 6. The body piece 32 has a peripheral rim 38, which is fitted in the open end of the annular rim 350.

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A fourth embodiment of the present invention will now be described with reference to Figs. 7 and 8 mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. As shown in Figs. 7 and 8, the inner end face 37 of the head end wall 30 has a first tapered face 375, which joins the inner wall surface 351 of the annular rim 35, a second tapered surface 376, which is joined to the first tapered surface 375 and a flat central surface 377, which is joined to the second tapered surface 376. If the piston 17 is cut along the plane S, the tapered surfaces 375 and 376 have linear profiles. The closer a point on the first tapered surface 375 is to the axis L, the closer that point is to the outer end face 36. The closer a point on the second tapered surface 376 is to the axis L, the further that point is from the outer end face 36.

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Next, a fifth embodiment of the present invention will be described with reference to Figs. 9(a) and 9(b) mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. In this embodiment, the head piece 31 has a plate-like head end wall 40, as shown in Figs. 9(a) and 9(b). The head end wall 40 has an inner end face 41 that is planar and parallel to the outer end face 36.

As shown in Fig. 9(b), the inner end face 41 has a plurality of integral reinforcing ribs 39 (six ribs in this embodiment). The reinforcing ribs 39 extend radially from the axis L and are arranged at 60° angular intervals. Inner end portions 391 of the reinforcing ribs 39 are located at the axis L, and outer end portions 392 of the reinforcing ribs 39 are connected to the inner wall surface 351 of the annular rim 35. The inner end portions 391 are axially aligned with the positioning recess 361. The rear face 393 of each reinforcing rib 39 is parallel to the outer end face 36 of the head end wall 40. In other words, the thickness of each reinforcing rib 39 (as measured in the direction of the axis L) is the same over its entire length.

This embodiment has the following advantages.

25 The reinforcing ribs 39 formed on the inner end face 41 increase the surface area on the rear side of the head end wall 30. This reduces stress concentration in the head end wall 40 and limits the weight of the head end wall 40 compared with the case where the thickness of the head end wall is increased uniformly. Thus, the head end wall 40 is strong and is lighter than a simple plate-like head end wall.

The reinforcing ribs 39 reduces the concentration of stress in their longitudinal directions. The reinforcing ribs

39 extend radially from the axis L of the head end wall 40. This reduces the concentration of stress in the head end wall 40.

The connection of all the reinforcing ribs 39 to the inner wall surface 351 of the annular rim 35 reduces the concentration of stress between the annular rim 35 and the head end wall 40.

The inner end portions 391 of all the reinforcing ribs 39 are located at the axis L. This improves the strength of the head end wall 40 around the axis L. Further, the inner end portions 391 are aligned axially with the positioning recess 361. This compensates for the loss of strength in the head end wall 40 attributed to the positioning recess 361.

The reinforcing ribs 39 are arranged around the axis L at equiangular intervals. This reduces the concentration of circumferential stress in the head end wall 40.

The head piece 31 is formed by die casting, cutting or press molding. The two-piece structure facilitates formation of the reinforcing ribs 39 on the inner end face 41 of the head end wall 40.

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A sixth embodiment of the present invention will be described with reference to Figs. 10(a) and 10(b) mainly in terms of the differences from the embodiment shown in Figs. 9(a) and 9(b). In this embodiment, a plurality of reinforcing ribs 42 are formed on the inner end face 41 of the head end wall 40. Each reinforcing rib 42 extends not from the axis L but from a point offset from the axis L and is connected to the inner wall surface 351 of the annular rim 35. The reinforcing ribs 42 are arranged around the axis L at

equiangular intervals. The inner end portions 421 of the reinforcing ribs 42 define a rectangular box surrounding the axis L. The piston of the sixth embodiment has the same advantages as that of the embodiment shown in Figs. 9(a) and 9(b).

A seventh embodiment of the present invention will be described with reference to Figs. 11(a) and 11(b) mainly in terms of the differences from the embodiment shown in Figs. 9(a) and 9(b). The piston of this embodiment is like that of the embodiment of Figs. 9(a) and 9(b), except that only four reinforcing ribs 43 are formed on the inner end face 41 of the head end wall 40 and that the ribs 43 are not connected to the inner wall surface 351 of the annular rim 35.

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An eighth embodiment of the present invention will be described with reference to Figs. 12(a) and 12(b) mainly in terms of the differences from the embodiment shown in Figs. 9(a) and 9(b). In this embodiment, a protrusion 44 is formed on the inner end face 41 of the head end wall 40. The protrusion 44 is centered on the axis L. The protrusion 44 corresponds only to the inner end portions 391 of the reinforcing ribs 39 in Fig. 9(a). The protrusion 44 has a substantially cylindrical shape. The protrusion 44 is smoothly joined to the inner end face 41.

A ninth embodiment of the present invention will be described with reference to Figs. 13(a) and 13(b) mainly in terms of the differences from the embodiment shown in Figs. 12(a) and 12(b). In this embodiment, a protrusion 45 is

formed on the inner end face 41 of the head end wall 40. The protrusion 45 has a ring-like form and is centered on the axis L.

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A tenth embodiment of the present invention will be described with reference to Figs. 14(a) and 14(b) mainly in terms of the differences from the embodiment shown in Figs. 12(a) and 12(b). In this embodiment, the protrusion 44 and four reinforcing ribs 46 are formed on the inner end face 41 of the head end wall 40. The protrusion 44 is substantially the same as that shown in Fig. 12(a). The reinforcing ribs 46 extend radially from the protrusion 44 and are connected to the inner wall surface 351 of the annular rim 35. The reinforcing ribs 46 are arranged around the axis L at equiangular intervals.

The protrusion 44 may be omitted to leave only the reinforcing ribs 46.

An eleventh embodiment of the present invention will be described with reference to Figs. 15(a) and 15(b) mainly in terms of the differences from the embodiment shown in Figs. 12(a) and 12(b). This embodiment is substantially the same as the embodiment shown in Figs. 12(a) and 12(b), except that a plurality of reinforcing ribs 47 are included. The reinforcing ribs 47 each have a triangular plate-like form and are located in the corner formed between the inner end face 41 of the head end wall 40 and the inner wall surface 351 of the annular rim 35. The reinforcing ribs 47 extend radially and

The protrusion 44 may be omitted to leave only the reinforcing ribs 47.

are arranged around the axis L at equiangular intervals.

A twelfth embodiment of the present invention will be described with reference to Figs. 16(a) and 16(b) mainly in terms of the differences from the embodiment shown in Figs. 15(a) and 15(b). This embodiment is different from that shown

in Figs. 15(a) and 15(b) in that the protrusion 44 is replaced with a plurality of reinforcing ribs 48. The reinforcing ribs 48 each have a triangular plate-like form and extend radially from the axis L at equiangular intervals.

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The radially outer reinforcing ribs 47 may be omitted to leave only the radially inner reinforcing ribs 48.

A thirteenth embodiment of the present invention will be described with reference to Figs. 17(a) and 17(b) mainly in terms of the differences from the embodiment shown in Figs. 9(a) and 9(b). This embodiment is different from that shown in Figs. 9(a) and 9(b) in that the top face of each reinforcing rib 49 is curved, and that the number of the reinforcing ribs 49 is different from that of the embodiment shown in Figs. 9(a) and 9(b). The rear face 491 of each reinforcing rib 49 includes a concave surface 492 and a convex surface 493. The contour of the rear face 491, from the end of the inner wall surface 351 toward the axis L, first approaches the outer end face 36 and then departs from it.

A fourteenth embodiment of the present invention will be described with reference to Figs. 18(a) and 18(b) mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. This embodiment is different from that shown in Figs. 1 to 4 in that the protrusion 50 has a flat end face. The protrusion 50 extends from an annular concave surface 371, which smoothly joins the inner wall surface 351 of the annular rim 35. An annular convex surface 378 is smoothly joined to the concave portion 371, and a flat face 379 smoothly joins the annular convex surface 378. The annular convex surface 378 is a part of a sphere. The closer a point on the annular convex surface 378 is to the axis L, the further that point is from the outer end face 36. The flat face 379 is parallel to

the outer end face 36.

A fifteenth embodiment of the present invention will be described with reference to Figs. 19 and 20 mainly in terms of the differences from the embodiment shown in Figs. 1 to 4. This embodiment is substantially the same as that shown in Figs. 1 to 4, except that a plurality of reinforcing ribs 60 are included. The reinforcing ribs 60 (four ribs in this embodiment) extend radially from the axis L and are connected to the inner wall surface 351 of the annular rim 35. The rear surface 601 of each reinforcing rib 60 is parallel to the outer end face 36. The reinforcing ribs 60 further improve the strength of the head end wall 30 compared with the embodiment shown in Figs. 1 to 4.

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A sixteenth embodiment of the present invention will be described with reference to Figs. 21 and 22 mainly in terms of the differences from the embodiment shown in Figs. 19 and 20. This embodiment is substantially the same as the embodiment shown in Figs. 19 and 20, except that reinforcing ribs 70 each have a curved rear surface 701. The rear surface 701 is curved to match the contour of the inner end face 37 of the head end wall 30. In this embodiment, the quantity of material necessary for forming the reinforcing ribs 70 is reduced compared with the embodiment shown in Figs. 19 and 20.

Next, a process for producing the head piece 31 shown in Figs. 18(a) and 18(b) will be described with reference to Figs. 23(a) and 23(b). Fig. 23(a) shows a first mold 51 and a second mold 52, which are used for casting the head piece 31. The first mold 51 has a portion that does not conform to the shape of the inner end face 37 of the head end wall 30. More specifically, the first mold 51 is designed and formed such that it forms an extra protrusion 54 on the inner end face 37.

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The protrusion 54 is not present in the finished product. A pushing rod 53 is fitted to the first mold 51 to move axially.

The molds 51 and 52 are mated with each other, and in this state molten metal, based on aluminum, is poured into a casting space between the molds 51 and 52. Before the molten metal in the molds 51 and 52 solidifies, the pushing rod 53 is urged in the axial direction Q shown in Fig. 23(a). Thus, the molten metal present in the portion corresponding to the extra protrusion 54 is pushed by the distal end of the pushing rod 53. This prevents formation of shrinkage cavities in a workpiece 310, which results after solidification of the molten metal.

After the molten metal is solidified, the workpiece 310 is taken out from the molds 51 and 52. A recess 541 matching the shape of the distal end of the pushing rod 53 remains in the extra protrusion 54. Subsequently, as shown in Fig. 23(b), the extra protrusion 54 is removed by cutting with a cutting tool 55 such as an end mill. The portion of the inner end face 37 from which the extra protrusion 54 is removed forms the flat face 379 (see Fig. 18(a)).

According to the above production process, shrinkage
25 cavities in the head piece 31 can be prevented. This improves
the strength of the head piece 31.

The extra protrusion 54 may not be cut off completely. In this case, the remaining extra protrusion 54 serves as an annular reinforcing rib.

The following embodiments are within the scope of the present invention.

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In the embodiment shown in Figs. 1 to 4, the curvature of the inner end face 37 of the head end wall 30 is not limited to the illustration but can be modified suitably. Further, the inner end face 37 of the head end wall 30 may be formed by a combination of curved surfaces and tapered surfaces. For example, a tapered surface may be located between the annular concave portion 371 and the inner wall surface 351 of the annular rim 35, or a tapered surface may be located between the annular groove-like surface 371 and the convex surface 372.

In the embodiment shown in Figs. 1 to 4, the convex portion 372 may not be a part of a spherical face but may be of any type as long as it has a smooth curved surface.

In the embodiment shown in Figs. 7 and 8, the flat central surface 377 may be replaced with a conical tapered surface 376 having an apex centered on the axis L.

A recess may be formed on the flat central surface 377 shown in Fig. 7 or on the flat face 379 shown in Fig. 18(a).

The first piston member may be connected to the second piston member using an adhesive.

The first piston member may be connected to the second piston member by means of friction pressure.

The first piston member may be connected to the second piston member by means of press fitting.

In the piston in any of the foregoing embodiments, a positioning recess 361 is formed on the outer end face of the head end wall. However, the present invention can be applied

in those pistons that have no positioning recesses 361. Light and strong hollow pistons can be obtained again in such cases.

Therefore, the present examples and embodiments are to be considered as illustrative and not restrictive, and the invention is not to be limited to the details given herein, but may be modified within the scope or equivalence of the appended claims.